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# Microstructure Optimization of the MIP-177-LT Membrane for Highly Efficient Uranium Separation from Seawater

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# 1. INTRODUCTION

separation from seawater.

To promote the goal of carbon neutrality, nuclear power has been identified as a promising energy source.<sup>1–3</sup> However, land-based uranium fuel reserves are limited to ~6.3 million tons and will face a severe shortage in less than 100 years.<sup>4–6</sup> Fortunately, there are about 4.5 × 10<sup>9</sup> tons of uranium resources in seawater,<sup>7,8</sup> providing a solution to the current uranium shortage. Nonetheless, the complicated composition of seawater poses a challenge to high-efficiency uranium purification.<sup>9–12</sup> One the one hand, a large number of interfering metal ions (e.g., Fe<sup>3+</sup>, Mg<sup>2+</sup>, Ca<sup>2+</sup>, Na<sup>+</sup>, and K<sup>+</sup>) coexist in nature seawater, rendering high-efficiency separation of trace amounts of UO<sub>2</sub><sup>2+</sup> ions (3.3 ppm) very challenging;<sup>11,13,14</sup> on the other hand, the salinity of seawater (3.2–4.0 wt %) is ~10<sup>6</sup> times higher than UO<sub>2</sub><sup>2+</sup> ions,<sup>13,15,16</sup> significantly hindering the efficiency of uranium separation.

63.4  $L \cdot m^{-2} \cdot h^{-1} \cdot bar^{-1}$ , revealing great potential in practical uranium

Diverse protocols, including adsorption,  $^{11,17-21}$  photocatalysis,  $^{6,22-28}$  ion exchange,  $^{29-31}$  solvent extraction,  $^{32-34}$ electrochemical precipitation,  $^{35-37}$  and membrane,  $^{38,39}$  have been studied for the uranium separation from seawater. Among them, membrane technology has attracted much attention because of the high efficiency, low energy requirement, operation simplicity, and eco-friendliness.  $^{15,16,40}$  Aiming at achieving high-efficiency uranium separation from seawater, accurate discrimination of UO<sub>2</sub><sup>2+</sup> ions from coexisting interfering ions (e.g., Fe<sup>3+</sup>, Mg<sup>2+</sup>, Ca<sup>2+</sup>, Na<sup>+</sup>, and K<sup>+</sup>) has become indispensable. Since hydrated kinetic diameters of

hydrated metal ions in seawater are in the order  $K^+(6.6 \text{ Å}) <$  $Na^{+}(7.2 \text{ Å}) < Ca^{2+}(8.2 \text{ Å}) < Mg^{2+}(8.6 \text{ Å}) < Fe^{3+}(9.1 \text{ Å}) <$  $UO_2^{2+}(11.6 \text{ Å})$ , the selection of microporous membranes with pore size ranging between hydrated diameters of UO2<sup>2+</sup> ions and other metal ions (e.g., 10–11 Å) is preferred.  $\overline{41,42}$  In principle, the rejection rate of  $UO_2^{2+}$  ions should be as high as possible (ideally 100%), while that of other metal ions should be as low as possible (ideally, 0%). GO-based membranes have been employed in uranium separation from seawater. The rejection rate of  $UO_2^{2+}$  ions in simulated seawater was ~100%; however, the rejection rate of other ions remained relatively high (>10%); simultaneously, water permeance of GO-based membranes was relatively low, which could be due to the high tortuosity of the pore channels in 2D membranes, resulting in a high diffusion barrier.<sup>43,44</sup> Therefore, both the pore size and preferred orientation of microporous membranes should be deliberately tailored.

Metal-organic frameworks (MOFs), a class of porous crystalline materials composed of regularly arranged metal ions/metal-oxo clusters and organic ligands, have been

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Figure 1. Schematic illustration of the synthesis of the MIP-177-LT membrane toward uranium separation from natural seawater.

regarded as excellent membrane candidates for molecular sieving because of their tunable pore size, rich functional groups, and high surface areas.<sup>4,40,45-48</sup> Among them, MIP-177-LT, which consists of Ti12O15 units interconnected by 3,3',5,5'-tetracarboxydiphenylmethane (H<sub>4</sub>mdip) ligands and interconnecting formate groups, features a three-dimensional pore system with 11 Å hexagonal-shaped pores extending along the c axis (Figure S3c,d).<sup>49,50</sup> Since its pore size just falls between the kinetic diameters of UO<sub>2</sub><sup>2+</sup> ions and other smallersized metal ions (e.g., Fe<sup>3+</sup> ions), the fabrication of a preferentially c-oriented MIP-177-LT membrane would be promising for high-efficiency uranium separation from seawater; moreover, relying on the coupling effect between the 3 Å sized channel along the b axis and the 11 Å sized channel along the c axis, versatile water permeation channels can be provided, which is beneficial for achieving higher water permeance.

In this study, we fabricated the highly *c*-orientated MIP-177-LT membrane through epitaxial growth (Figure 1).<sup>51</sup> Since the growth rate of MIP-177-LT crystallites along the c-orientation was faster than other orientations, according to the van der Drift evolution principle, MIP-177-LT crystallites evolving along the c-direction would prevent the growth of other crystallites along other directions, leading to the formation of a preferentially c-oriented MIP-177-LT membrane. Relevant ion rejection experiment data showed that the obtained membrane exhibited a  $UO_2^{2+}$  rejection rate of 98.3% with a water permeance of 44.6  $L \cdot m^{-2} \cdot h^{-1} \cdot bar^{-1}$ ; in contrast, the rejection rate of  $M^{n+}$  (M = K, Na, Ca, and Mg, n = 1 and 2) was below 6%. Of particular note, the  $Fe^{3+}$  rejection rate was only 41.4%. To the best of our knowledge, such a large rejection discrepancy between UO2<sup>2+</sup> and Fe<sup>3+</sup> has been rarely reported in the literature.

## 2. EXPERIMENTAL SECTION

**2.1. Preparation of MIP-177-LT Nanoseeds.** 5,5'-Methylenediisophthalic acid (H<sub>4</sub>mdip, 100 mg, 0.29 mmol, Shanghai Tensus Biotech Co., Ltd.) was added into formic acid (10 mL) and dispersed by sonication at 25 °C for 15 min. Titanium isopropoxide (TPOT, 300  $\mu$ L, 0.99 mmol) was added dropwise to the above precursor suspension under sonication. Following sonication for 15 min, the above suspension was poured into a 30 mL Teflon-lined autoclave and solvothermally treated at 110 °C for 24 h. After repeated washing with ethanol, the solid product was finally dried in an oven at 60 °C overnight.

**2.2. Preparation of the MIP-177-LT Seed Layer.** Dip coating was implemented to deposit the MIP-177-LT seed layer. MIP-177-LT seed suspension (4 mg/mL) was prepared by adding 120 mg of MIP-177-LT nanoseeds in 30 mL of MeOH. Subsequently, 20  $\mu$ L of PVP solution (0.01 mmol/L, solvent is DMF) was added to the suspension and stirred for 3 days before using. Then, a porous  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> tube was immersed in MIP-177-LT nanoseed suspension for 20 s and slowly lifted out. The operation was repeated twice. Finally, the seed layer was dried at 60 °C for 12 h.

2.3. Preparation of the MIP-177-LT Membrane.  $H_4$ mdip (80 mg) was added to 25 mL of formic acid and sonicated for 10 min until complete dissolution of the ligand. Then, 400  $\mu$ L of TPOT was added to the above precursor suspension under vigorous stirring. After 15 min of sonication, the suspension was transferred to a 60 mL Teflon-lined autoclave in which the MIP-177-LT seed layer was vertically placed. Finally, the Teflon-lined autoclave was treated at 110 °C for 25 h. After cooling, the as-prepared MIP-177-LT membrane was washed with DI water overnight before use.



Figure 2. SEM images of (a, b) MIP-177-LT seeds, (c, d) MIP-177-LT seed layer, and (e, f) MIP-177-LT membrane. (g) XRD patterns of MIP-177-LT seeds, seed layer, and membrane. (h) digital photos of the  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> substrate, MIP-177-LT seed layer, and MIP-177-LT membrane. Scale bars: 2  $\mu$ m.

# 3. RESULTS AND DISCUSSION

**3.1. Preparation of MIP-177-LT Seeds.** MIP-177-LT nanoseeds were synthesized in the first step, which could be facilely prepared through reported literature.<sup>52</sup> As shown in Figure 2a, the obtained rod-shaped seeds exhibited an aspect ratio of ~1.6 (Figure 2b) with size distribution ranging between 250 and 350 nm (Figure S4a,b). Relevant XRD patterns were consistent with the standard MIP-177-LT phase (Figure S5). N<sub>2</sub> adsorption/desorption isotherms indicated that their BET surface areas and micropore volume reached 526.98 m<sup>2</sup>·g<sup>-1</sup> and 0.3812 cm<sup>3</sup>·g<sup>-1</sup> (Figure S6), respectively, which were comparable with those in the reported literature.

Considering the high salinity, complex composition, and varying temperature of seawater, the robustness of MIP-177-LT crystallites in aqueous solution was further evaluated under varying pH values (1–4 and 10) and temperatures. As shown in Figure S7, the morphology of MIP-177-LT crystallites did not change under the above harsh conditions. XRD patterns and FT-IR spectra showed that there was no variation in phase purity and functionality (Figures S8 and S9), while TGA data showed that there was no significant weight loss of up to 400 °C (Figure S10). Therefore, the obtained MIP-177-LT crystallites exhibited excellent chemical and thermal stability, which was beneficial to withstand long-term exposure to natural seawater.

**3.2. Preparation of the MIP-177-LT Seed Layer and Relevant Membrane.** Subsequently, we attempted to deposit a uniform MIP-177-LT seed layer through dip coating. The results showed that the addition of PVP represented the key factor to maintain the uniformity of the MIP-177-LT seed layer. Obviously, the addition of PVP in seed suspension weakened mutual interactions between adjacent MIP-177-LT seeds, resulting in enhanced dispersion in suspension.<sup>53,54</sup> As shown in Figure S11, MIP-177-LT nanoseeds were uniformly deposited on porous  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> tubes upon maintaining a seed solution concentration of 2–5 mg/mL; nonetheless, further increasing seed concentration would lead to severe aggregation in the seed layer. As shown in Figure 2c,d, the thickness of the randomly oriented MIP-177-LT seed layer reached 1.9  $\mu$ m.

The next step referred to epitaxial growth for sealing the open space in the seed layer. According to the van der Drift evolution mechanism, since the growth rate of MIP-177-LT crystallites along the *c*-orientation was faster than other orientations, when they met, MIP-177-LT crystallites growing closer to the *c*-orientation would prevent further growth of the ones evolving along other orientations. Eventually, bc-/ac-faces of MIP-177-LT crystallites tended to arrange in a direction perpendicular to the substrate surface, which led to the formation of the preferentially *c*-orientated MIP-177-LT membrane.<sup>51,52</sup> Our results revealed that increasing the

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**Figure 3.** (a) Long-term CR rejection test of the MIP-177-LT membrane. (b) Metal ion transmission rate of the MIP-177-LT membrane as a function of the ionic diameter. (c) Single metal ion separation performance of the MIP-177-LT membrane. (d) Ideal selectivity of  $M^{n+}$  (n = 1, 2, and 3)/UO<sub>2</sub><sup>2+</sup> ion pairs. (e) Binary metal ion separation performance of the MIP-177-LT membrane. (f) SF of binary  $M^{n+}$  (n = 1, 2, and 3)/UO<sub>2</sub><sup>2+</sup> ion pairs.

 $H_4$ mdip concentration ( $\leq 4 \text{ mg/mL}$ ) was beneficial for increasing the degree of c-orientation of MIP-177-LT membranes (Figure S12).55 Under optimized conditions, a well-intergrown MIP-177-LT membrane with a thickness of 3.1  $\mu$ m was obtained (Figure 2e,f). The cross-sectional image showed that the membrane thickness was increased by 63.15% compared with the seed layer, revealing that the epitaxial growth along the out-of-plane direction was triggered to a large extent.<sup>56-58</sup> The relevant XRD pattern exhibited a significant diffraction peak at a  $2\theta$  value of 7.1°, corresponding to the (001) plane of the MIP-177-LT phase (Figure 2g). The crystallographic preferred orientation (CPO) index has been widely employed to quantify the degree of preferred orientation of crystallites in the membrane. In this study, the  $CPO_{(001)/(100)}$  index, in which  $I_M$  and  $I_P$  belonged to the intensity of (001) and (100) plane reflections, respectively, was employed to evaluate the degree of the *c*-preferred orientation of the MIP-177-LT membranes (shown in Figure S8). Our results indicated that compared with the MIP-177-LT seed layer, the  $CPO_{(001)/(100)}$  index of the MIP-177-LT membrane significantly increased to 8.4, indicating the dominance of the preferred c-orientation of MIP-177-LT crystallites in the membrane, which was beneficial for the concurrent increase

in rejection rate and water permeance due to the appropriate pore size and minimized diffusion path length.

3.3. Ion Rejection Test of the MIP-177-LT Membrane. Before the ion rejection test, the continuity of our membrane was assessed with a 25 Å sized Congo Red (CR, Figure S14) rejection test. A CR rejection rate of ~99% was achieved with a water permeance of 37  $L \cdot m^{-2} \cdot h^{-1} \cdot bar^{-1}$ , indicating the existence of a few grain boundary defects in the membrane (Figure 3a). Subsequently, the ion rejection capacity of the obtained MIP-177-LT membrane was evaluated. We first measured the single ion rejection capacity of the membrane. Since the pore size of MIP-177-LT in the *c*-axis direction fell between  $UO_2^{2+}$  ions and other smaller-sized metal ions, an accurate screening of  $UO_2^{2+}$  ions could be realized (Figure 3b). As shown in Figure 3c, the rejection rate of  $UO_2^{2+}$  ions of our membrane reached 98.3%, which was much higher than those of K<sup>+</sup> (4.5%), Na<sup>+</sup> (5.1%), Ca<sup>2+</sup> (5.3%), Mg<sup>2+</sup> (5.7%), and Fe<sup>3+</sup> ions (41.4%), implying that size-based exclusion represented the dominant mechanism for metal ion rejection; correspondingly, the ideal selectivities of  $K^+/UO_2^{2+}$ ,  $Na^+/UO_2^{2+}$ ,  $Ca^{2+}/$  $UO_2^{2+}$ ,  $Mg^{2+}/UO_2^{2+}$ , and  $Fe^{3+}/UO_2^{2+}$  ion pairs reached 44.5, 44.4, 43.9, 42.8, and 29.86, respectively (Figure 3d). It should be noted that in sharp contrast to the high rejection rate of



**Figure 4.** (a) Comparison of the selectivity of binary  $M^{n+}$  (n = 1 and 2)/UO<sub>2</sub><sup>2+</sup> ion pairs of the MIP-177-LT membrane with other materials (Tables S1 and S2). (b) Comparison of rejection rates of UO<sub>2</sub><sup>2+</sup> and Fe<sup>3+</sup> ions as well as the SF of binary Fe<sup>3+</sup>/UO<sub>2</sub><sup>2+</sup> ion pairs of the MIP-177-LT membrane with other materials reported in the literature (Table S3).



**Figure 5.** Uranium separation capacity of the MIP-177-LT membrane under natural seawater conditions. (a) Concentrations of the main metal ions from the Yellow Sea at Dalian; (b) rejection rates of various metal ions; (c) selectivity of  $M^{n+}$  (n = 1, 2, and 3)/UO<sub>2</sub><sup>2+</sup> ion pairs under natural seawater conditions.

 $\mathrm{UO_2}^{2+}$  ions, rejection rates of M<sup>+</sup> and M<sup>2+</sup> ions were remarkably lower (<6%), which was advantageous for accurately screening  $UO_2^{2+}$  ions from other high-concentration interfering metal ions. We also noticed that there was a remarkable difference between rejection rates of Fe<sup>3+</sup> and  $UO_2^{2+}$  ions. We have recently reported the preparation of MOF-808 membranes with the rejection rate of Fe<sup>3+</sup> ions reaching 98.3%, which was remarkably higher than that of MIP-177-LT membranes.<sup>59</sup> Such a large discrepancy in rejection rates of Fe<sup>3+</sup> ions could be attributed to the slightly larger pore size of the MIP-177-LT membrane, resulting in a higher diffusion rate of Fe<sup>3+</sup> ions through the membrane with negligible influence on the  $Fe^{3+}/UO_2^{2+}$  selectivity; simultaneously, the water permeance of the K<sup>+</sup> ion-containing solution reached 63.4  $L \cdot m^{-2} \cdot h^{-1} \cdot bar^{-1}$ . As far as we know, this represented the highest value reported in the literature for pure MOF membranes, which could be attributed to (i) minimized diffusion path length in the membrane, (ii) versatile channels enabling fast permeation of water molecules, and (iii) hydrophilicity of the MIP-177-LT membrane surface (Figure S15). As expected, the water permeance generally decreased with increasing hydrated kinetic diameters of metal ions, which could be rationally interpreted by the size-exclusion effect (Figure 3c).

We further evaluated the binary metal ion separation capacity of the obtained MIP-177-LT membrane. As shown in Figure 3c, compared with single metal ions, there was a slight increase in rejection rate in the presence of  $UO_2^{2+}$  ions.

For instance, the rejection rate of K<sup>+</sup> ions reached 5.7% in the presence of UO<sub>2</sub><sup>2+</sup> ions, which was slightly higher than that of single  $K^+$  ions (Figure 3e). This may be due to the strong coupling effect between metal ions and competitive diffusion in the channel, giving rise to higher ion-permeable free energy barriers.  ${}^{60,61}$  To be specific, the separation factors (SFs) of K<sup>+</sup>/UO<sub>2</sub><sup>2+</sup>, Na<sup>+</sup>/UO<sub>2</sub><sup>2+</sup>, Ca<sup>2+</sup>/UO<sub>2</sub><sup>2+</sup>, Mg<sup>2+</sup>/UO<sub>2</sub><sup>2+</sup>, and Fe<sup>3+</sup>/UO<sub>2</sub><sup>2+</sup> ion pairs reached 40.6, 39.1, 37.7, 32.7, and 19.5, respectively (Figure 3f) with water permeance largely unchanged (58.89, 45.64, 29.30, 27.52, and 19.63 L·m<sup>-2</sup>·h<sup>-1</sup>·  $bar^{-1}$ ) (Figure 3e). It should be noted that in comparison with the literature (Figure 4a), our membrane displayed efficient UO2<sup>2+</sup> interception and screening precision toward versatile metal ions  $(M^{n+}/UO_2^{2+}, n = 1 \text{ and } 2)$  while maintaining high water permeance, which had been rarely reported in the literature (Tables S1 and S2); moreover, in comparison with the literature, our membrane exhibited the largest difference between rejection rates of  $Fe^{3+}$  and  $UO_2^{2+}$  ions (Figure 4b and Table S3).

Targeting practical applications, we further investigated the uranium rejection capacity of the MIP-177-LT membrane under natural seawater conditions. According to the literature, uranium in natural seawater mainly exists in the form of  $UO_2^{2+}$  ions.<sup>11,62,63</sup> Concentrations of major metal ions in the Yellow Sea are as follows (Figure 5a): Na<sup>+</sup> (~8528 ppm) > Mg<sup>2+</sup> (~1077 ppm) > K<sup>+</sup> (~335 ppm) ~ Ca<sup>2+</sup> (~351 ppm) > Fe<sup>3+</sup> (~0.15 ppm) > UO\_2^{2+} (~0.14 ppm). Our results showed that the uranium rejection rate reached 97.6%, which was

comparable to the rejection rate of single UO<sub>2</sub><sup>2+</sup> ions, while rejection rates of other smaller-sized metal ions only slightly increased, indicating a negligible influence on the separation efficiency (Figure 5b). Correspondingly, our membrane exhibited satisfying selectivity toward K<sup>+</sup>/UO<sub>2</sub><sup>2+</sup> (36.2), Na<sup>+</sup>/UO<sub>2</sub><sup>2+</sup> (33.1), Ca<sup>2+</sup>/UO<sub>2</sub><sup>2+</sup> (33.0), Mg<sup>2+</sup>/UO<sub>2</sub><sup>2+</sup> (32.1), and Fe<sup>3+</sup>/UO<sub>2</sub><sup>2+</sup> (18.6) ion pairs with a water permeance of 14.43 L·m<sup>-2</sup>·h<sup>-1</sup>·bar<sup>-1</sup> (Figure 5c), showing great promise for high-efficiency uranium separation from natural seawater.

# 4. CONCLUSIONS

In this study, a preferentially *c*-oriented MIP-177-LT membrane was fabricated on a porous  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> tube. Relying on 11 Å sized channels arranged along the *c* axis, the obtained membrane achieved a rejection rate of 98% for UO<sub>2</sub><sup>2+</sup> ions. In contrast, rejection rates as low as <6% were achieved in terms of small-sized hydrated monovalent and divalent metal ions; simultaneously, the largest difference between rejection rates of Fe<sup>3+</sup> and UO<sub>2</sub><sup>2+</sup> ions in comparison with the literature was achieved in terms of pure MOF membranes. Under natural seawater conditions, the rejection rate of UO<sub>2</sub><sup>2+</sup> ions reached 97.6% with a water permeance of 14.4 L·m<sup>-2</sup>·h<sup>-1</sup>·bar<sup>-1</sup>, holding great promise for practical uranium separation from nature seawater with balanced UO<sub>2</sub><sup>2+</sup> selectivity and water permeance.

#### ASSOCIATED CONTENT

#### **1** Supporting Information

The Supporting Information is available free of charge at https://pubs.acs.org/doi/10.1021/acs.iecr.5c01651.

Additional experimental details, experimental reagents, detailed characterizations of MIP-177-LT powders and membranes, and relevant test details (PDF)

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# **Author Contributions**

The manuscript was written through contributions of all authors. All authors have given approval to the final version of the manuscript. Y.Z. performed the major experiments and analyzed the experimental data. M.Y. and T.W. helped with the experiments on uranium rejection under natural seawater conditions. S.C. and J.J. helped with the experiments on CR rejection. M.W. helped with the analysis of experimental data. S.W., S.-i.N., and X.Z. helped with the compilation of the manuscript. J.L. and J.M. helped with the hydrophilic angle measurements and Congo Red dye diagram drawing. Y.L. and Y.Z. cowrote the manuscript with contributions from all authors.

#### Notes

The authors declare no competing financial interest.

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